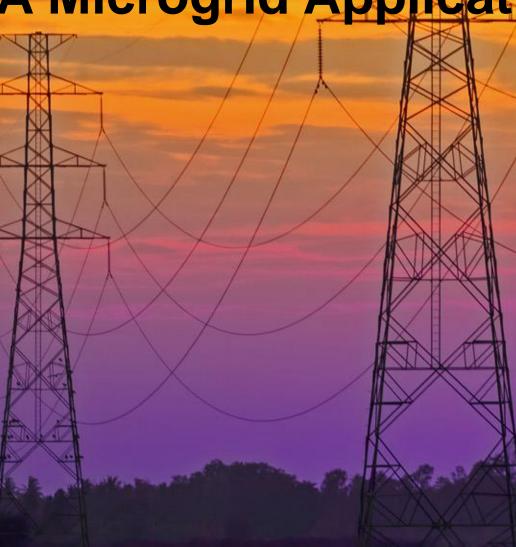


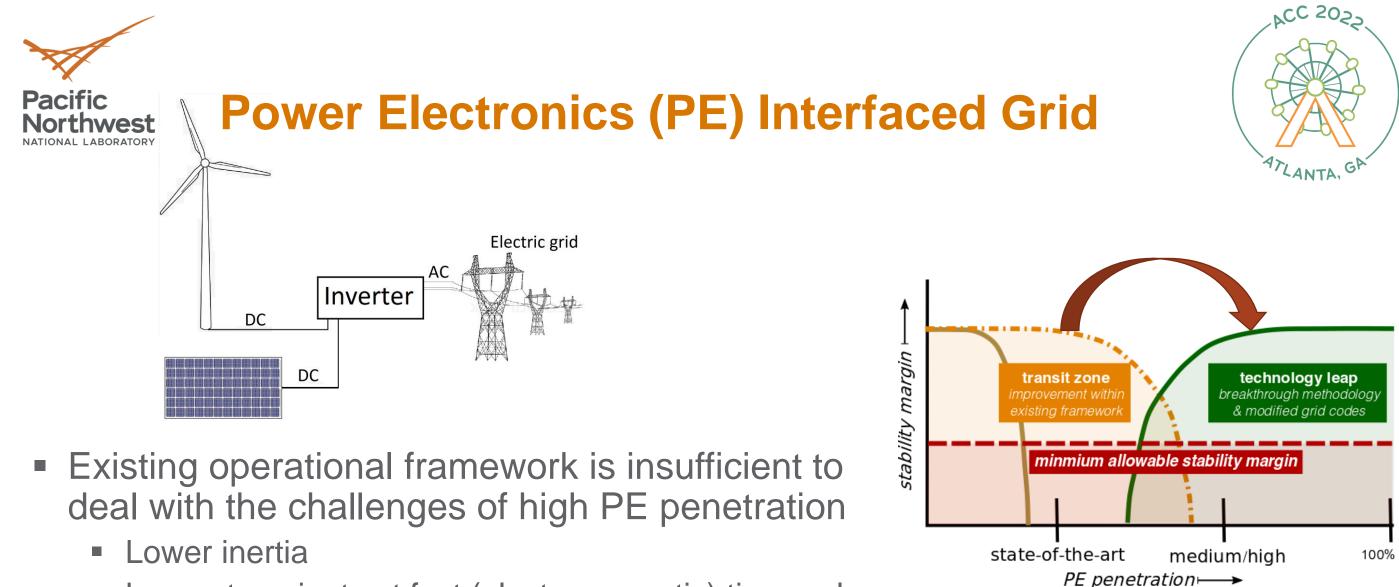
# **Distributed Transient Safety Verification via Robust Control** Invariant Sets: A Microgrid Application

Jean-Baptiste Bouvier, Sai Pushpak Nandanoori, **Melkior Ornik and Soumya Kundu** 





June 9, 2022



- - Larger transients at fast (electromagnetic) timescales
  - Higher uncertainties in power generation
  - Reduced stability and safety margins

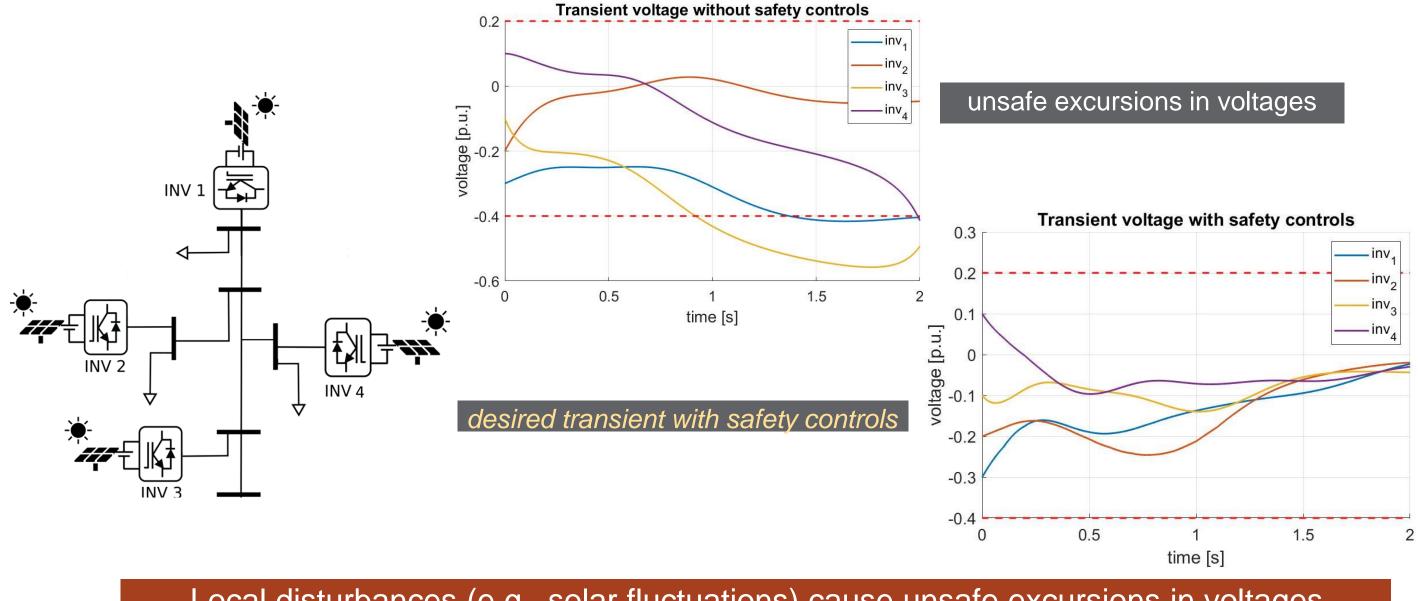
### ... need transformational change to achieve extreme high PE penetration (>75%)

### \*Source: EU MIGRATE Report

### **Problem: Local Transient Safety Constraints**

Pacific

Northwest

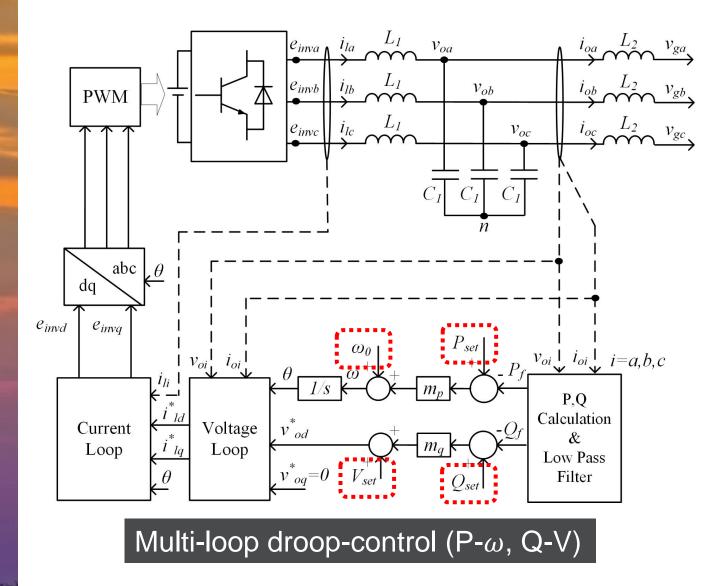


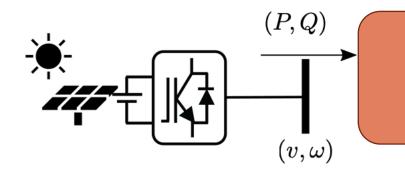
Local disturbances (e.g., solar fluctuations) cause unsafe excursions in voltages





### **Emerging Technologies: Grid-Forming Inverters**





- Grid-forming inverters
  - Provides virtual inertia; acts as a voltage source; stable synchronization via inner control loops; black-start, and more ...
- Multi-loop droop-control regulates voltage and frequency by controlling power (P,Q)

$$\omega_{\text{set}} = \omega_{\text{set}}^* - \lambda_p (P - P_q)$$
 $v_{\text{set}} = v_{\text{set}}^* - \lambda_q (Q - Q_q)$ 

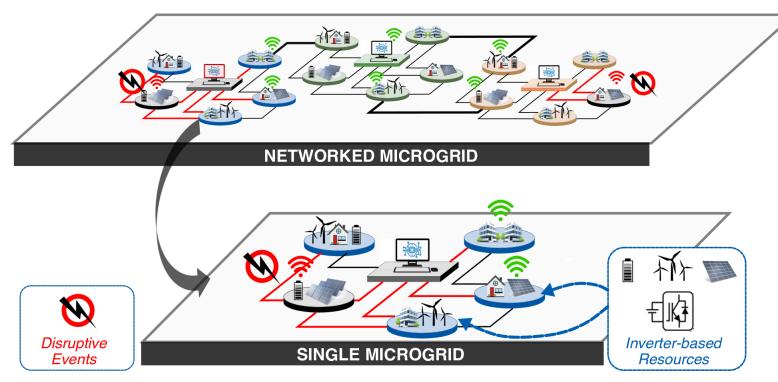




 $\mathbf{P}_{\text{set}}$ (*P*- $\omega$  droop) (Q-V droop)  $\mathbf{set}$  )

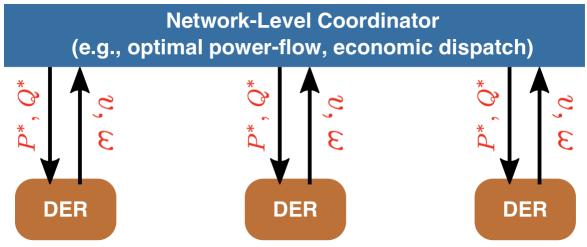


### **Hierarchical and Distributed Framework**



- Hierarchical and distributed (DERs) over the network
- Individual resources (e.g., points to track

**Example**: Optimal Power-Flow - DERs receive set-points; in turn regulates voltage and frequency







# operations to coordinate many distributed energy resources

# inverters) received control set-



### **Multi-timescales Problem**

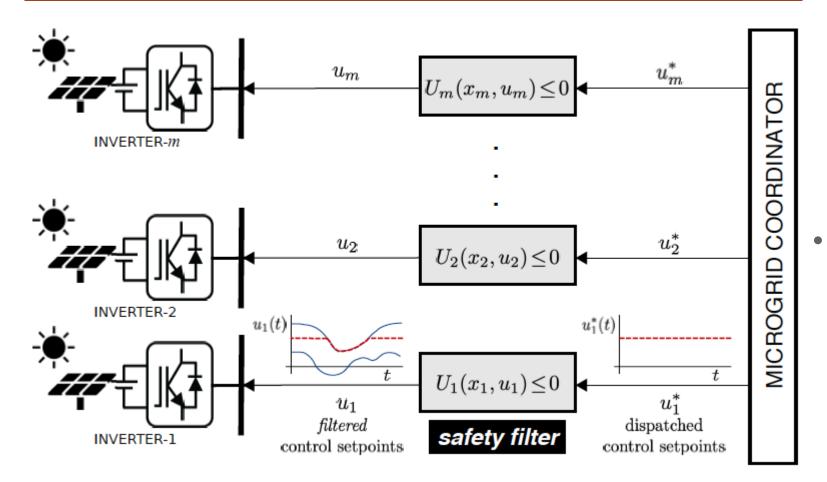
State-of-the-art operational practices in inverter-based microgrids lack the spatiotemporal granularity required to proactively prevent transient safety and stability violations which are often local and fast-evolving in nature.





### **Safety Filter: The Concept**

Decouple network-level objectives from local transient safety constraints





7

### Safety filters are deployed locally at the inverter terminals, and act as gatekeepers for allowable (safe) set-points

State-inclusive bounds on the allowable control set-points

In a robust design, guarantees transient safety constraint satisfaction under bounded uncertainties in the network



### **Droop-controlled inverter dynamics**

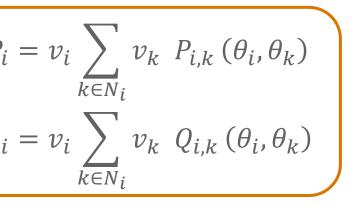
Local  
dynamics  
$$\begin{aligned} & \dot{\theta}_i = \omega_i \\ \tau_i \dot{\omega}_i = -\omega_i + \lambda_i^p (P_i^0 + u_i^p - P_i) \\ \tau_i \dot{\nu}_i = \nu_i^0 - \nu_i + \lambda_i^q (Q_i^0 + u_i^q - Q_i) \end{aligned} \qquad \begin{bmatrix} P_i \\ Q_i \end{bmatrix} \\ \textbf{Controls} \quad u_i^p \text{ and } u_i^q \end{aligned}$$

**Safe sets**  $S_v = [v, \overline{v}]$ , and  $S_\omega = [\omega, \overline{\omega}]$ .

**Local measurements**  $\theta_i, \omega_i, v_i$  are known,  $P_i$  and  $Q_i$  are unknown.

**Problem** How to maintain  $v \in S_v$  and  $\omega \in S_\omega$  during transients?





### ghbor interactions

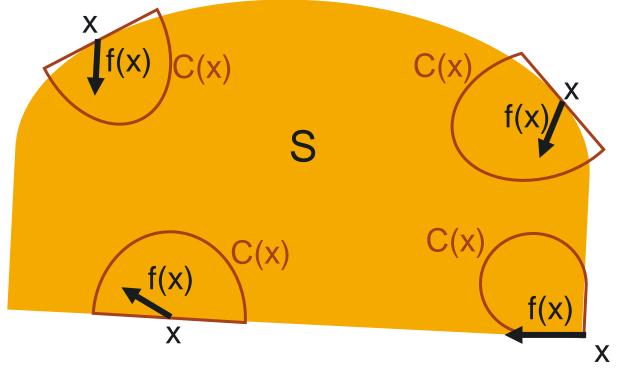


### **Invariant sets**

S is **invariant** by  $\dot{x} = f(x)$  if for all  $x(0) \in S$ ,  $x(t) \in S$  for  $t \ge 0$ .

### **Nagumo theorem**

A closed set S is invariant by  $\dot{x} = f(x)$ if and only if for all  $x \in S$ ,  $f(x) \in C(x)$ , the Bouligand tangent cone to S at x.



S is **robust control invariant** by  $\dot{x} = f(x, u, w)$ if there exists a control law u(t) such that for all  $x(0) \in S$  and all  $w \in W$ ,  $x(t) \in S$  for all  $t \ge 0$ .

Blanchini, "Set invariance in control," Automatica 1999.





# **Upper and lower invariance of safe sets**

 $S = [s, \overline{s}]$  is upper invariant (resp. lower invariant) for U by  $\dot{x} = f(x, u, w)$  if for all  $u \in U$ ,  $w \in W$  and all  $x(0) \in S$ ,  $x(t) \leq \overline{s}$  (resp.  $x(t) \geq s$ ) for all  $t \geq 0$ .

If  $\dot{x} = g(x, w) + \lambda u$  with  $\lambda > 0$ , we define a **minimal lower control** u and a **maximal upper control**  $\overline{u}$  such that

 $u = min\{u_{low} \in U : S \text{ is lower invariant for all } u \geq u_{low}\},\$ 

 $\overline{u} = \max\{u_{up} \in U : S \text{ is upper invariant for all } u \leq u_{up}\}.$ 

$$f(\underline{s}, u_{low}, w) \qquad S \qquad S$$

 $U = [u, \overline{u}]$  is the maximal interval of **safety admissible** controls making S robust control invariant.







## **Extremal upper and lower controls**

$$\overline{u_i^p} = \max_{\theta_k, v_k} \{ u_i^p : \dot{\omega}_i \le 0, \omega_i = \overline{\omega} \} = \max_{\theta_k, v_k} \frac{1}{\lambda_i^p} \overline{\omega_i} + P_i - P_i^0$$
s.t
$$\underline{u_i^p} = \min_{\theta_k, v_k} \{ u_i^p : \dot{\omega}_i \ge 0, \omega_i = \underline{\omega} \} = \min_{\theta_k, v_k} \frac{1}{\lambda_i^p} \underline{\omega_i} + P_i - P_i^0$$

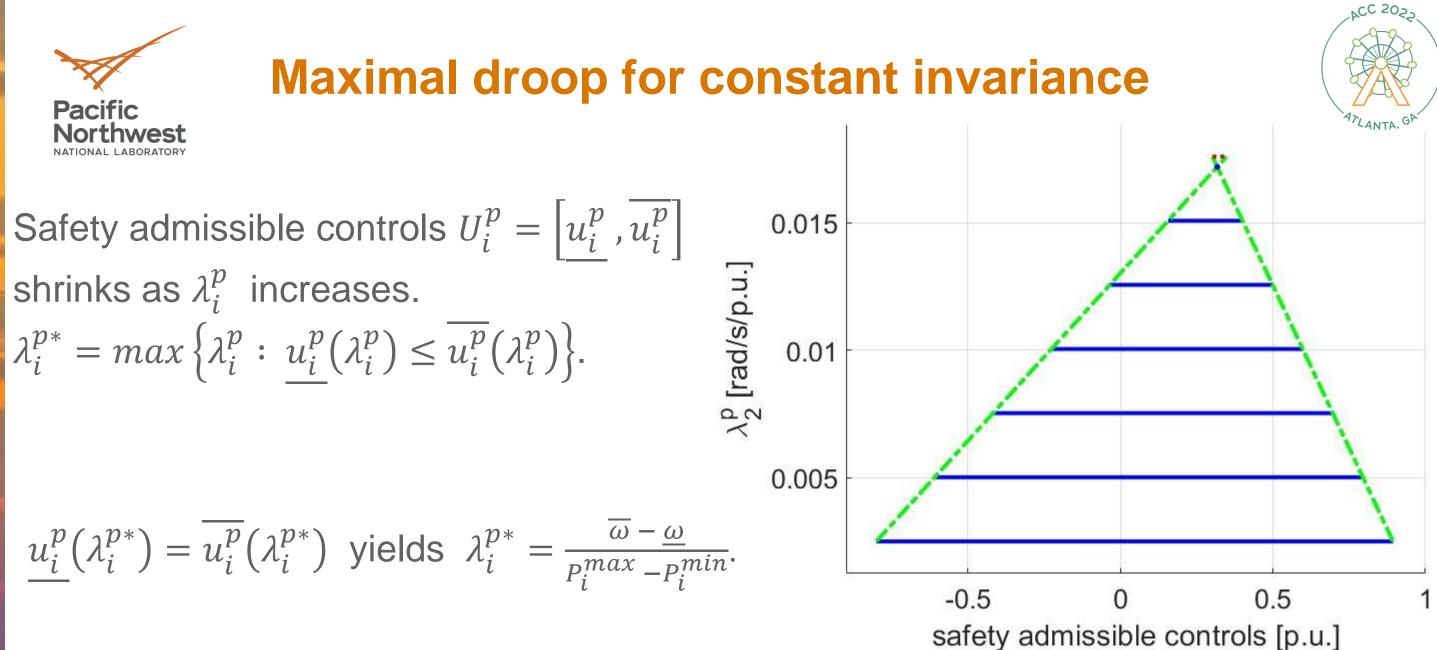
Only 
$$P_i$$
 depends on  $\theta_k$ ,  $v_k$ . Thus, let
$$\begin{aligned}
P_i^{max} &= \max_{\theta_k, v_k} \{P_i : \omega_i = \overline{\omega}\}, \\
P_i^{min} &= \min_{\theta_k, v_k} \{P_i : \omega_i = \underline{\omega}\}
\end{aligned}$$

So that 
$$\overline{u_i^p} = \frac{1}{\lambda_i^p}\overline{\omega} + P_i^{max} - P_i^0$$
 and  $\underline{u_i^p} = \frac{1}{\lambda_i^p}\underline{\omega} + P_i^{min} - P_i^0$ .



### t. $\theta_k \in S_{\theta}, v_k \in S_{v}$ for all $k \in N_i$ , and $S_{\theta} = [\underline{\theta}, \overline{\theta}]$ .

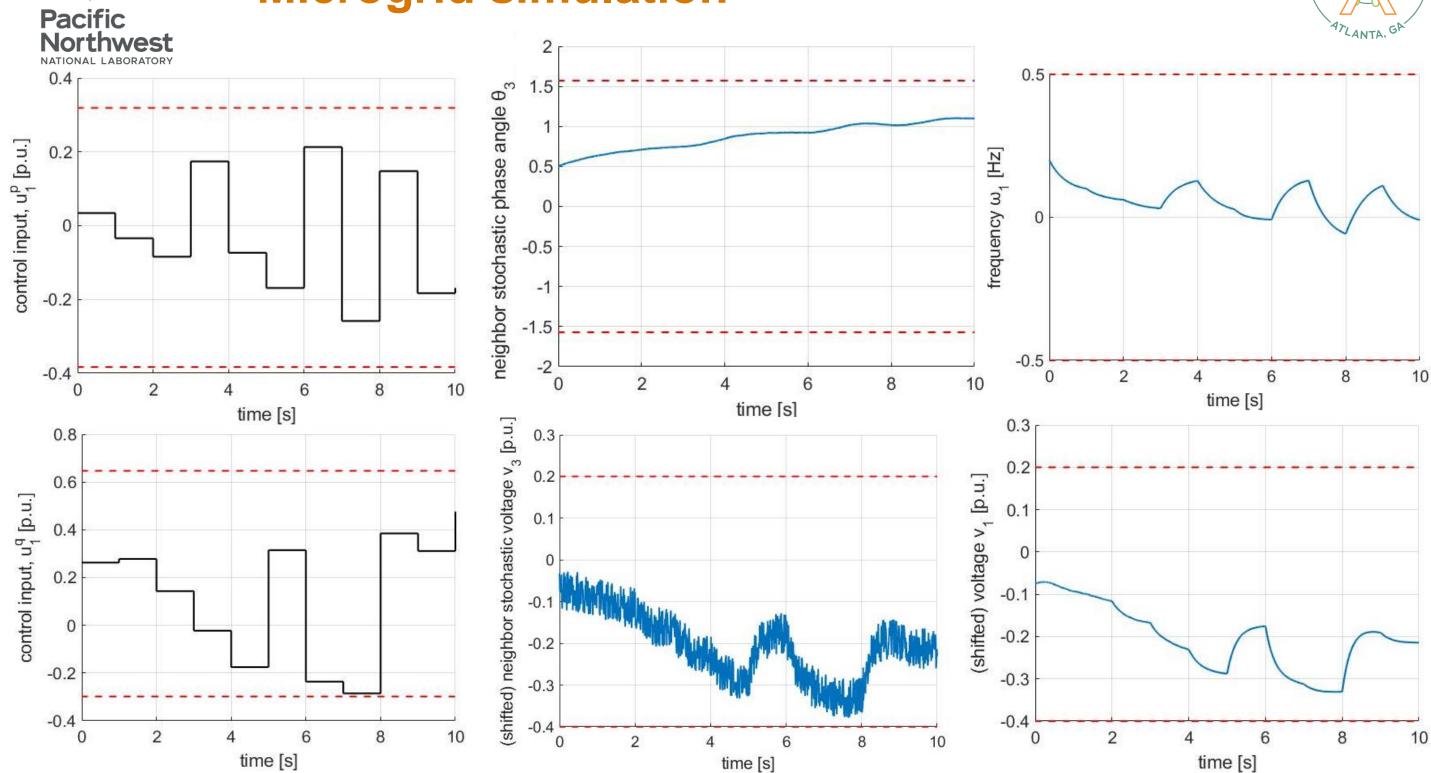




Sum-of-Squares algorithms to calculate  $P_i^{min} P_i^{max}$ .

Language & SDP solver	MATLAB SeDuMi	Julia SDPA	Julia Mosek
Run-time for $P_i^{min}$ , $P_i^{max}$	4295s ~1h12	343s ~ 6min	33s











### **Problem:** how to prevent transient safety violations in inverter-based microgrids?

**Solution:** we relied on Nagumo's theorem to ensure robust control invariance of the frequency and voltage safe sets.







# Thank you

